

Systèmes discrets linéaires et stationnaires

Solution

$$\begin{aligned} x(k+1) &= \Phi x(k) + \Gamma u(k) & x(k) &= \underbrace{\Phi^{k-k_0} x(k_0)}_{\text{Réponse libre}} + \underbrace{\sum_{l=k_0}^{k-1} \Phi^{k-l-1} \Gamma u(l)}_{\text{Réponse forcée}} \\ y(k) &= Cx(k) + Du(k) \end{aligned}$$

Matrice de transfert et stabilité

$$Y(z) = [C(zI - \Phi)^{-1} \Gamma + D] U(z) = H(z) U(z)$$

$$H(z) = \begin{bmatrix} H_{11}(z) & \dots & H_{1r}(z) \\ \vdots & & \vdots \\ H_{p1}(z) & \dots & H_{pr}(z) \end{bmatrix} = [H_{ij}(z)] = \left[\frac{H_{ij}^*(z)}{\det(zI - \Phi)} \right]$$

Pôles z_i des H_{ij} solution de: $\det(zI - \Phi) = 0$

Valeurs propres v_i de Φ solution de: $\det(\lambda I - \Phi) = 0$

$$z_i = v_i$$

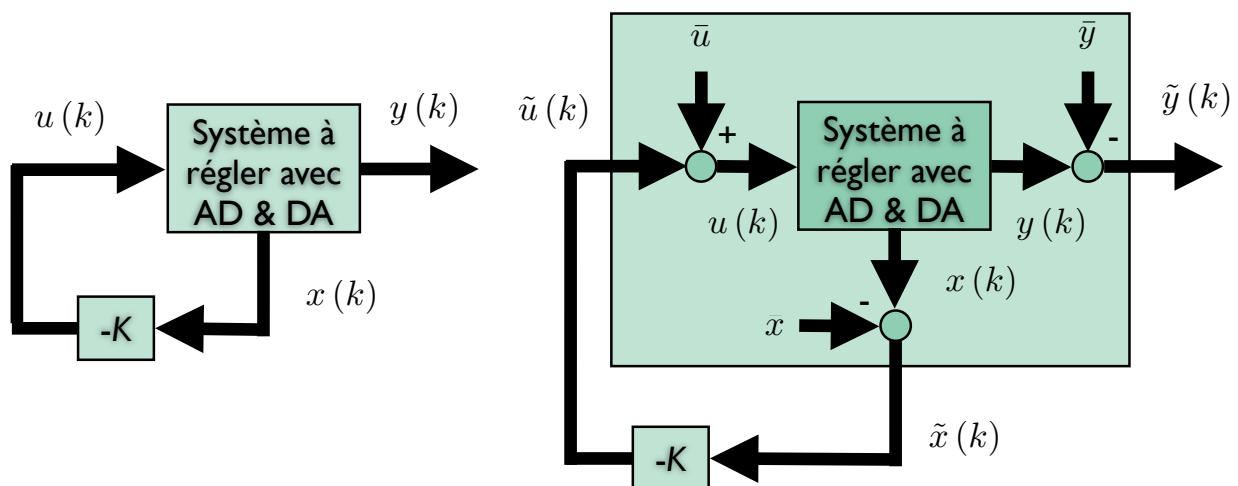
Asymptotiquement stable si: $|v_i| < 1$ pour $i = 1, \dots, n$

Tuesday, October 26, 2010

Commande d'état

$$\begin{array}{l} \text{Système} \\ \text{à régler} \end{array} \quad \begin{aligned} x(k+1) &= \Phi x(k) + \Gamma u(k) \\ y(k) &= Cx(k) + Du(k) \end{aligned} \quad \begin{aligned} \tilde{x}(k+1) &= \Phi \tilde{x}(k) + \Gamma \tilde{u}(k) \\ \tilde{y}(k) &= C\tilde{x}(k) + D\tilde{u}(k) \end{aligned}$$

$$\text{Régulateur} \quad u(k) = -Kx(k) \quad \tilde{u}(k) = -K\tilde{x}(k)$$



Commande d'état

Système à régler

$$\begin{aligned} x(k+1) &= \Phi x(k) + \Gamma u(k) \\ y(k) &= Cx(k) + Du(k) \end{aligned}$$

Régulateur

$$u(k) = -Kx(k)$$

Système en boucle fermée (BF)

$$\begin{aligned} x(k+1) &= \overbrace{(\Phi - \Gamma K)}^{\Phi_{BF}} x(k) \\ y(k) &= \underbrace{(C - DK)}_{C_{BF}} x(k) \end{aligned}$$

$$X(z) = (zI - \Phi_{BF})^{-1} zx(0) = W(z)x(0)$$

$$X_i(z) = W_{i1}(z)x_1(0) + \dots + W_{ij}(z)x_j(0) + \dots + W_{in}(z)x_n(0)$$

$$Z^{-1}[W_{ij}(z)] = \sum_i c_i z_i^k + 2 \sum_i |c_i^*| r_i^k \cos(k\omega_i + \varphi_i) + \sum_i [c_{1i}' z_i^k + c_{2i}' k z_i^{k-1} + \dots]$$

La commande d'état ramène l'état à zéro $x(k) \rightarrow 0$ pour $k \rightarrow \infty$

En variables écart, la commande d'état ramène l'état à l'état nominal $\tilde{x}(k) \rightarrow 0$ ou $x(k) \rightarrow \bar{x}$ pour $k \rightarrow \infty$

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Principe de synthèse de la commande d'état

Système à régler

$$\begin{aligned} x(k+1) &= \Phi x(k) + \Gamma u(k) \\ y(k) &= Cx(k) + Du(k) \end{aligned}$$

Régulateur

$$u(k) = -Kx(k)$$

Système en boucle fermée (BF)

$$\begin{aligned} x(k+1) &= \overbrace{(\Phi - \Gamma K)}^{\Phi_{BF}} x(k) \\ y(k) &= \underbrace{(C - DK)}_{C_{BF}} x(k) \end{aligned}$$

$$\begin{aligned} \det(\lambda I - \Phi_{BF}) &= \det(\lambda I - \Phi + \Gamma K) = \\ \alpha_c(\lambda) &= (\lambda - \lambda_1)(\lambda - \lambda_2) \dots (\lambda - \lambda_n) = \\ &= \lambda^n + \alpha_1 \lambda^{n-1} + \dots + \alpha_{n-1} \lambda + \alpha_n = 0 \end{aligned}$$

Identification terme à terme dans le cas SIMO (une entrée)

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Double intégrateur (5.1.2)

$$\begin{array}{l} \text{Système} \\ \text{en BF} \end{array} \quad \begin{array}{l} x(k+1) = \overbrace{(\Phi - \Gamma K)}^{\Phi_{BF}} x(k) \\ y(k) = \underbrace{(C - DK)}_{C_{BF}} x(k) \end{array} \quad \Phi = \begin{bmatrix} 1 & h \\ 0 & 1 \end{bmatrix} \quad \Gamma = \begin{bmatrix} h^2/2 \\ h \end{bmatrix}$$

$$\det(\lambda I - \Phi + \Gamma K) = (\lambda - \lambda_1)(\lambda - \lambda_2) = 0$$

Choix des valeurs propres

$$\lambda_{1,2} = 0.8 \pm 0.25j$$

$$\det \left(\begin{bmatrix} \lambda & 0 \\ 0 & \lambda \end{bmatrix} - \begin{bmatrix} 1 & h \\ 0 & 1 \end{bmatrix} + \begin{bmatrix} h^2/2 \\ h \end{bmatrix} \begin{bmatrix} K_1 & K_2 \end{bmatrix} \right) = (\lambda - 0.8 - 0.25j)(\lambda - 0.8 + 0.25j)$$

$$\det \left(\begin{bmatrix} \lambda - 1 + \frac{h^2}{2}K_1 & -h + \frac{h^2}{2}K_2 \\ hK_1 & \lambda - 1 + hK_2 \end{bmatrix} \right) = \lambda^2 - 1.6\lambda + 0.7$$

$$\lambda^2 + \underbrace{\left(hK_2 + \frac{h^2}{2}K_1 - 2 \right)}_{-1.6} \lambda + \underbrace{\left(\frac{h^2}{2}K_1 - hK_2 + 1 \right)}_{0.7} = \lambda^2 - 1.6\lambda + 0.7$$

$$K_1 = 0.1/h^2 = 10 \quad \text{et} \quad K_2 = 0.35/h = 3.5 \quad \text{pour} \quad h = 0.1s$$

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FT → Modèle d'état (2.5)

$$H(z) = \frac{Y(z)}{U(z)} = \frac{b_0 + b_1z^{-1} + b_2z^{-2} + \dots + b_nz^{-n}}{1 + a_1z^{-1} + a_2z^{-2} + \dots + a_nz^{-n}}$$

$$w(k+1) = \underbrace{\begin{bmatrix} -a_1 & -a_2 & \dots & -a_{n-1} & -a_n \\ 1 & 0 & \dots & 0 & 0 \\ 0 & 1 & & \vdots & \vdots \\ \vdots & & \ddots & 0 & 0 \\ 0 & \dots & 0 & 1 & 0 \end{bmatrix}}_{\Phi_w} w(k) + \underbrace{\begin{bmatrix} 1 \\ 0 \\ \vdots \\ 0 \\ 0 \end{bmatrix}}_{g_w} u(k)$$

$$y(k) = \underbrace{\left[b_1 - a_1b_0 \quad b_2 - a_2b_0 \quad \dots \quad b_n - a_nb_0 \right]}_{c_w^T} w(k) + b_0u(k)$$

$$\det(\lambda I - \Phi_w) = \lambda^n + a_1\lambda^{n-1} + a_2\lambda^{n-2} + \dots + a_n\lambda + a_n = 0$$

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Modèle d'état physique → artificiel (A.I.2)

$$\left| \begin{array}{l} x(k+1) = \Phi x(k) + gu(k) \\ y(k) = c^T x(k) + du(k) \end{array} \right. \quad \text{Transformation} \quad \left| \begin{array}{l} w = Px \\ x = P^{-1}w \end{array} \right.$$

$$\left| \begin{array}{l} P^{-1}w(k+1) = \Phi P^{-1}w(k) + gu(k) \\ y(k) = c^T P^{-1}w(k) + du(k) \end{array} \right.$$

$$\left| \begin{array}{l} w(k+1) = P\Phi P^{-1}w(k) + Pgu(k) \\ y(k) = c^T P^{-1}w(k) + du(k) \end{array} \right.$$

Quelle matrice de transformation P choisir ?

$$\left| \begin{array}{l} w(k+1) = \underbrace{P\Phi P^{-1}}_? w(k) + \underbrace{Pg}_? u(k) \\ y(k) = \underbrace{c^T P^{-1}}_? w(k) + du(k) \end{array} \right.$$

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Modèle d'état physique → artificiel

$$G = [Ig \quad \Phi g \quad \dots \quad \Phi^{n-1}g] \quad G^{-1} = \begin{bmatrix} e_1^T \\ e_2^T \\ \vdots \\ e_n^T \end{bmatrix} \quad P = \begin{bmatrix} e_n^T \Phi^{n-1} \\ e_n^T \Phi^{n-2} \\ \vdots \\ e_n^T I \end{bmatrix}$$

Construction de Pg

$$I = G^{-1}G = \begin{bmatrix} 1 & 0 & \dots & 0 \\ 0 & 1 & \ddots & \vdots \\ \vdots & \ddots & \ddots & 0 \\ 0 & \dots & 0 & 1 \end{bmatrix} = \begin{bmatrix} e_1^T Ig & e_1^T \Phi g & \dots & e_1^T \Phi^{n-1}g \\ e_2^T Ig & e_2^T \Phi g & \dots & e_2^T \Phi^{n-1}g \\ \vdots & \vdots & & \vdots \\ e_n^T Ig & e_n^T \Phi g & & e_n^T \Phi^{n-1}g \end{bmatrix}$$

$$Pg = \begin{bmatrix} e_n^T \Phi^{n-1}g \\ e_n^T \Phi^{n-2}g \\ \vdots \\ e_n^T Ig \end{bmatrix} = \begin{bmatrix} 1 \\ 0 \\ \vdots \\ 0 \end{bmatrix}$$

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Modèle d'état physique → artificiel

$$I = PP^{-1} = \begin{bmatrix} e_n^T \Phi^{n-1} \\ e_n^T \Phi^{n-2} \\ \vdots \\ e_n^T I \end{bmatrix} P^{-1} = \begin{bmatrix} 1 & 0 & \dots & 0 \\ 0 & 1 & \ddots & \vdots \\ \vdots & \ddots & \ddots & 0 \\ 0 & \dots & 0 & 1 \end{bmatrix} = \begin{bmatrix} e_n^T \Phi^{n-1} P^{-1} \\ e_n^T \Phi^{n-2} P^{-1} \\ \vdots \\ e_n^T P^{-1} \end{bmatrix}$$

Construction de

$$P\Phi P^{-1} = \begin{bmatrix} e_n^T \Phi^{n-1} \\ e_n^T \Phi^{n-2} \\ \vdots \\ e_n^T I \end{bmatrix} \Phi P^{-1} = \begin{bmatrix} e_n^T \Phi^n P^{-1} \\ e_n^T \Phi^{n-1} P^{-1} \\ \vdots \\ e_n^T \Phi P^{-1} \end{bmatrix} = \begin{bmatrix} -a_1 & -a_2 & \dots & -a_{n-1} & -a_n \\ 1 & 0 & \dots & 0 & 0 \\ 0 & 1 & & \vdots & \vdots \\ \vdots & & \ddots & 0 & 0 \\ 0 & \dots & 0 & 1 & 0 \end{bmatrix}$$

$$e_n^T \Phi^n P^{-1} = \begin{bmatrix} -a_1 & -a_2 & \dots & -a_{n-1} & -a_n \end{bmatrix}$$

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Modèle d'état physique → artificiel

$$G = \begin{bmatrix} Ig & \Phi g & \dots & \Phi^{n-1} g \end{bmatrix} \quad G^{-1} = \begin{bmatrix} e_1^T \\ e_2^T \\ \vdots \\ e_n^T \end{bmatrix} \quad P = \begin{bmatrix} e_n^T \Phi^{n-1} \\ e_n^T \Phi^{n-2} \\ \vdots \\ e_n^T I \end{bmatrix}$$

$$w = Px$$

$$w(k+1) = \underbrace{\begin{bmatrix} -a_1 & -a_2 & \dots & -a_{n-1} & -a_n \\ 1 & 0 & \dots & 0 & 0 \\ 0 & 1 & & \vdots & \vdots \\ \vdots & & \ddots & 0 & 0 \\ 0 & \dots & 0 & 1 & 0 \end{bmatrix}}_{\Phi_w = P\Phi P^{-1}} w(k) + \underbrace{\begin{bmatrix} 1 \\ 0 \\ \vdots \\ 0 \\ 0 \end{bmatrix}}_{g_w = Pg} u(k)$$

$$y(k) = \underbrace{\begin{bmatrix} b_1 - a_1 b_0 & b_2 - a_2 b_0 & \dots & b_n - a_n b_0 \end{bmatrix}}_{c_w^T = c^T P^{-1}} w(k) + b_0 u(k)$$

$$\det(\lambda I - \Phi_w) = \det(\lambda I - \Phi) = \lambda^n + a_1 \lambda^{n-1} + a_2 \lambda^{n-2} + \dots + a_n \lambda + a_n = 0 \quad 10$$

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Commande d'état

Système à régler	$\begin{aligned} x(k+1) &= \Phi x(k) + \Gamma u(k) \\ y(k) &= Cx(k) + Du(k) \end{aligned}$	SIMO $\Gamma = g$
Commande	$u(k) = -Kx(k)$ $x(k+1) = (\Phi - \Gamma K)x(k) = \Phi_{BF}x(k)$	
Stabilité en BO	$\det(\lambda I - \Phi) = \lambda^n + a_1\lambda^{n-1} + \dots + a_{n-1}\lambda + a_n = 0$	
Stabilité en BF	$\det(\lambda I - \Phi_{BF}) = \lambda^n + \alpha_1\lambda^{n-1} + \dots + \alpha_{n-1}\lambda + \alpha_n =$	
v.p. imposées	$\det(\lambda I - \Phi + \Gamma K) = (\lambda - \lambda_1)(\lambda - \lambda_2)\dots(\lambda - \lambda_n) = \alpha_c(\lambda) = 0$	
Méthode constructive	$w = Px \quad w(k+1) = (\Phi_w - \Gamma_w K')w(k) = \Phi_{wBF}w(k)$ $\alpha'_c(\lambda) = \alpha_c(\lambda) = 0 =$ $\det(\lambda I - \Phi_{wBF}) = \lambda^n + \alpha_1\lambda^{n-1} + \dots + \alpha_{n-1}\lambda + \alpha_n =$ $\det(\lambda I - \Phi_w + \Gamma_w K') = \lambda^n + (a_1 + K'_1)\lambda^{n-1} + \dots + (a_{n-1} + K'_{n-1})\lambda + (a_n + K'_n)$ $K'_i = \alpha_i - a_i \quad u(k) = -K'w(k) = -\underbrace{K'P}_K x(k)$	

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Formule d'Ackermann

$$K = K'P = [(\alpha_1 - a_1) \quad (\alpha_2 - a_2) \quad \dots \quad (\alpha_n - a_n)] P$$

$$K = [\alpha_1 \quad \alpha_2 \quad \dots \quad \alpha_n] P + \underbrace{[-a_1 \quad -a_2 \quad \dots \quad -a_n]}_{e_n^T \Phi^n P^{-1}} P$$

$$K = [\alpha_1 \quad \alpha_2 \quad \dots \quad \alpha_n] \begin{bmatrix} e_n^T \Phi^{n-1} \\ e_n^T \Phi^{n-2} \\ \vdots \\ e_n^T I \end{bmatrix} + e_n^T \Phi^n$$

$$K = e_n^T \Phi^n + \alpha_1 e_n^T \Phi^{n-1} + \alpha_2 e_n^T \Phi^{n-2} + \dots + \alpha_n e_n^T I$$

$$K = [e_n^T] \underbrace{[\Phi^n + \alpha_1 \Phi^{n-1} + \alpha_2 \Phi^{n-2} + \dots + \alpha_n I]}_{\alpha_c(\Phi)}$$

$$K = [0 \quad 0 \quad \dots \quad 0 \quad 1] G^{-1} \alpha_c(\Phi)$$

$$K = [0 \quad 0 \quad \dots \quad 0 \quad 1] [Ig \mid \Phi g \mid \dots \mid \Phi^{n-1} g]^{-1} \alpha_c(\Phi)$$

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Résumé Commande d'état SIMO

$$\begin{aligned} \text{Système à régler} \quad x(k+1) &= \Phi x(k) + gu(k) \\ y(k) &= Cx(k) + Du(k) \end{aligned}$$

$$\text{Commande} \quad u(k) = -Kx(k)$$

$$\text{Système en boucle fermée (BF)} \quad x(k+1) = (\Phi - gK)x(k) = \Phi_{BF}x(k)$$

$$\begin{aligned} \alpha_c(\lambda) &= \det(\lambda I - \Phi_{bf}) = (\lambda - \lambda_1)(\lambda - \lambda_2) \dots (\lambda - \lambda_n) \\ &= \lambda^n + \alpha_1 \lambda^{n-1} + \dots + \lambda a_{n-1} + \alpha_n = 0 \end{aligned}$$

Formule d'Ackermann

$$\begin{aligned} K &= [0 \ \dots \ 0 \ 1] G^{-1} \alpha_c(\Phi) \\ &= [0 \ \dots \ 0 \ 1] [Ig \ | \ \Phi g \ | \ \dots \ | \ \Phi^{n-1}g]^{-1} \alpha_c(\Phi) \end{aligned}$$

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Double intégrateur (5.3.1)

$$\begin{aligned} \text{Système en BF} \quad x(k+1) &= \overbrace{(\Phi - \Gamma K)}^{\Phi_{BF}} x(k) & \Phi &= \begin{bmatrix} 1 & h \\ 0 & 1 \end{bmatrix} & \Gamma &= \begin{bmatrix} h^2/2 \\ h \end{bmatrix} \\ y(k) &= \underbrace{(C - DK)}_{C_{BF}} x(k) \end{aligned}$$

$$\text{Choix des valeurs propres} \quad \lambda_{1,2} = 0.8 \pm 0.25j$$

$$\det(\lambda I - \Phi + \Gamma K) = (\lambda - \lambda_1)(\lambda - \lambda_2) = \lambda^2 - 1.6\lambda + 0.7$$

$$K = [0 \ 1] [Ig \ | \ \Phi g]^{-1} \alpha_c(\Phi)$$

$$K = [0 \ 1] \begin{bmatrix} h^2/2 & | & 3h^2/2 \\ h & | & h \end{bmatrix}^{-1} [\Phi^2 - 1.6\Phi + 0.7I]$$

$$K = [0 \ 1] \frac{1}{h^3} \begin{bmatrix} -h & | & 3h^2/2 \\ h & | & -h^2/2 \end{bmatrix} \left\{ \begin{bmatrix} 1 & h \\ 0 & 1 \end{bmatrix}^2 - 1.6 \begin{bmatrix} 1 & h \\ 0 & 1 \end{bmatrix} + 0.7 \begin{bmatrix} 1 & 0 \\ 0 & 1 \end{bmatrix} \right\}$$

$$K = \frac{[h \ -h^2/2]}{h^3} \begin{bmatrix} 0.1 & 0.4h \\ 0 & 0.1 \end{bmatrix} = \begin{bmatrix} \frac{0.1}{h^2} & \frac{0.35}{h} \end{bmatrix} = [K_1 \ K_2]$$

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Double intégrateur (5.3.1)

```

% Modèle discret

h = 0.1;

phi = [ 1 h ;
        0 1 ];

g = [ h^2/2 ;
      h ];

% Matrice de gouvernabilité

G = [ g phi*g];

% Coefficient du polynôme caractéristique en BF

alpha1 = -1.6;

alpha2 = 0.7;

% Gain de contre-réaction

K = [0 1] * inv(G) * (phi^2 + alpha1 * phi + alpha2 * eye(2));

% Calcul direct avec Ackermann

L = [0.8+0.25*i  0.8-0.25*i];

Kbis = acker(phi,g,L);
    
```

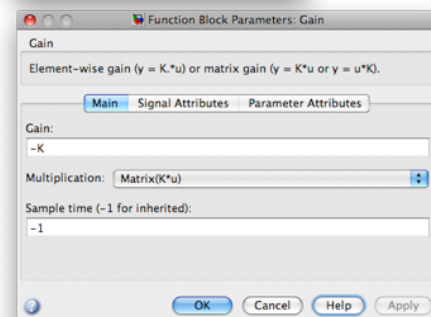
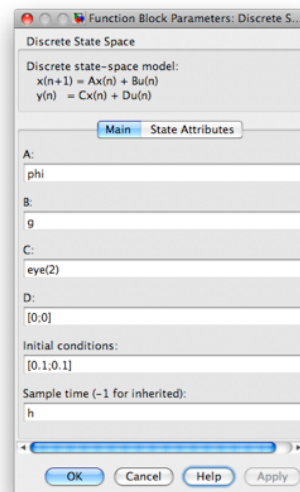
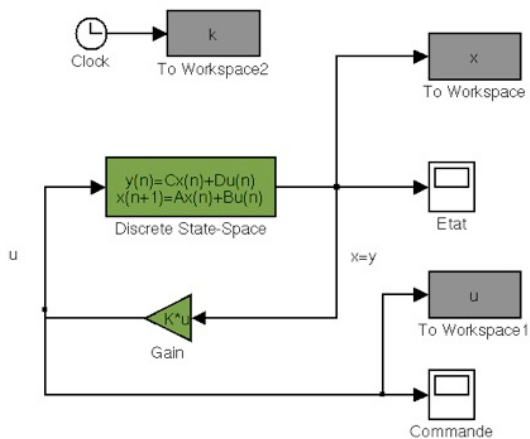
Code Matlab

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Double intégrateur (5.3.1)

Simulation avec Simulink



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Double intégrateur (5.3.1)

